# The Frenet–Serret formulas\*

Attila Máté Brooklyn College of the City University of New York

January 19, 2017

## Contents

Co	ntents	1
1	The Frenet–Serret frame of a space curve	1
<b>2</b>	The Frenet–Serret formulas	3
3	The first three derivatives of r	3
4	Examples and discussion	4
4.1	The curvature of a circle	4
4.2	The curvature and the torsion of a helix	5

## 1 The Frenet–Serret frame of a space curve

We will consider smooth curves given by a parametric equation in a three-dimensional space. That is, writing bold-face letters of vectors in three dimension, a curve is described as  $\mathbf{r} = \mathbf{F}(t)$ , where  $\mathbf{F}'$ is continuous in some interval I; here the prime indicates derivative. The length of such a curve between parameter values  $t_0 \in I$  and  $t_1 \in I$  can be described as

(1) 
$$\sigma(t_1) = \int_{t_0}^{t_1} |\mathbf{F}'(t)| \, dt = \int_{t_0}^{t_1} \left| \frac{d\mathbf{r}}{dt} \right| \, dt$$

where, for a vector **u** we denote by  $|\mathbf{u}|$  its length; here we assume  $t_0$  is fixed and  $t_1$  is variable, so we only indicated the dependence of the arc length on  $t_1$ . Clearly,  $\sigma$  is an increasing continuous function, so it has an inverse  $\sigma^{-1}$ ; it is customary to write  $s = \sigma(t)$ . The equation

(2) 
$$\mathbf{r} = \mathbf{F}(\sigma^{-1}(s)) \qquad s \in J \stackrel{def}{=} \{\sigma(t) : t \in I\}$$

is called the re-parametrization of the curve  $\mathbf{r} = \mathbf{F}(t)$  ( $t \in I$ ) with respect to arc length. It is clear that J is an interval. To simplify the description, we will always assume that  $\mathbf{r} = \mathbf{F}(t)$  and  $s = \sigma(t)$ ,

<sup>\*</sup>Written for the course Mathematics 2201 (Multivariable Calculus) at Brooklyn College of CUNY.

so we will just use the variables  $\mathbf{r}$ , t, and s instead of using function notation. We will use prime to indicate the differentiation d/dt, while the differentiation d/ds will not be abbreviated. We will assume that  $\mathbf{r}' \neq 0$  for any  $t \in I$ ; then  $\mathbf{r}'$  is a tangent vector to the curve corresponding to the given parameter value t.<sup>1.1</sup>

By the fundamental Theorem of Calculus, equation (1) implies

(3) 
$$s' = \frac{ds}{dt} = \frac{d\sigma(t)}{dt} = |\mathbf{F}'(t)| = |\mathbf{r}'|.$$

Hence, by the chain rule of differentiation we have

(4) 
$$\frac{d}{ds} = \frac{dt}{ds}\frac{d}{dt} = \left(\frac{1}{ds/dt}\right)\frac{d}{dt} = \frac{1}{|\mathbf{r}'|}\frac{d}{dt}$$

where the second equation follows from equation (1) by the Fundamental Theorem of calculus. When using differential operator notation as in d/ds, everything after the differential operator up to the next + or - sign needs to be differentiated; the expression preceding the differential operator is not to be differentiated. The unit tangent vector **T** is defined as<sup>1.2</sup>

(5) 
$$\mathbf{T} \stackrel{def}{=} \frac{1}{|\mathbf{r}'|} \mathbf{r}' = \frac{d\mathbf{r}}{ds};$$

the second equation follows from equations (4). The curvature is defined as

(6) 
$$\kappa \stackrel{def}{=} \left| \frac{d\mathbf{T}}{ds} \right|$$

We will assume that  $\kappa \neq 0.^{1.3}$  The unit normal vector is defined as

(7) 
$$\mathbf{N} \stackrel{def}{=} \frac{1}{\kappa} \frac{d\mathbf{T}}{ds}$$

Note that  $|\mathbf{T}|^2 = \mathbf{T} \cdot \mathbf{T}$ , so by the product rule of differentiation,

(8) 
$$\frac{d\mathbf{T}}{ds} \cdot \mathbf{T} = \frac{1}{2} \left( \frac{d\mathbf{T}}{ds} \cdot \mathbf{T} + \mathbf{T} \cdot \frac{d\mathbf{T}}{ds} \right) = 0;$$

hence **T** is perpendicular to  $d\mathbf{T}/ds$ , and so **N** is perpendicular to **T**. The unit binormal vector is defined as

(9) 
$$\mathbf{B} \stackrel{def}{=} \mathbf{T} \times \mathbf{N}$$

The vectors  $\mathbf{T}$ ,  $\mathbf{N}$ ,  $\mathbf{B}$  form the basic unit vectors of a coordinate system especially useful for describing the the local properties of the curve at the given point. These three vectors form what is called the *Frenet–Serret frame*. Equation (9) implies that the vectors  $\mathbf{T}$ ,  $\mathbf{N}$ ,  $\mathbf{B}$  form a right-handed system of pairwise perpendicular unit vectors. Any cyclic permutation of these vectors also form a righthanded system of pairwise perpendicular unit vectors; therefore we have

(10) 
$$\begin{aligned} \mathbf{T} \times \mathbf{N} &= \mathbf{B}, \\ \mathbf{N} \times \mathbf{B} &= \mathbf{T}, \\ \mathbf{B} \times \mathbf{T} &= \mathbf{N}. \end{aligned}$$

<sup>&</sup>lt;sup>1.1</sup>If the equation  $\mathbf{r} = \mathbf{F}(t)$  describes a moving point, where t is time, then **r** is the velocity vector of the moving point at time t. That is, the length of **r'** is its speed, while the direction of r' is its direction of its movement. If  $\mathbf{r'} = 0$ , then the point stopped moving at the given time, and then it may resume its movement in a different direction. This means that even though the function **F** is differentiable, the tangent line to the curve described by the function may not be defined at this point.

 $<sup>^{1.2}</sup>$ A unit vector is a vector of length 1.

<sup>&</sup>lt;sup>1.3</sup>We will comment later on what happens when  $\kappa \neq 0$ .

#### The Frenet–Serret formulas $\mathbf{2}$

As  $|\mathbf{N}| = 1$ , we have  $|\mathbf{N}|^2 = \mathbf{N} \cdot \mathbf{N} = 1$ , and so, similarly to equation (8), we have

$$\frac{d\mathbf{N}}{ds} \cdot \mathbf{N} = 0.$$

That is  $d\mathbf{N}/ds$  is perpendicular to  $\mathbf{N}$ , so we have

(11) 
$$\frac{d\mathbf{N}}{ds} = \alpha \mathbf{T} + \tau \mathbf{B}$$

for some numbers  $\alpha$  and  $\tau$  (depending on t).<sup>2.1</sup> Here  $\tau$  is called the torsion of the curve at the point; the value of  $\alpha$  will be determined below. Using this equation, equations (10), and the product rule of differentiation for vector products, we have

(12) 
$$\frac{d\mathbf{B}}{ds} = \frac{d(\mathbf{T} \times \mathbf{N})}{ds} = \frac{d\mathbf{T}}{ds} \times \mathbf{N} + \mathbf{T} \times \frac{d\mathbf{N}}{ds}$$
$$= \kappa \mathbf{N} \times \mathbf{N} + \mathbf{T} \times (\alpha \mathbf{T} + \tau \mathbf{B}) = \tau \mathbf{T} \times \mathbf{B} = -\tau \mathbf{N};$$

the third equation follows by equations (6) and (11). The first term of the third member<sup>2.2</sup> is zero: so is first term after distributing the cross product in the second term in the third member. Thus the fourth equation follows; to obtain the last equation we used equation (10). Hence, using equation (10), we have

(13) 
$$\frac{d\mathbf{N}}{ds} = \frac{d(\mathbf{B} \times \mathbf{T})}{ds} = \frac{d\mathbf{B}}{ds} \times \mathbf{T} + \mathbf{B} \times \frac{d\mathbf{T}}{ds}$$
$$= -\tau \mathbf{N} \times \mathbf{T} + \mathbf{B} \times (\kappa \mathbf{N}) = \tau \mathbf{B} + \kappa \mathbf{B} \times \mathbf{N} = -\kappa \mathbf{T} + \tau \mathbf{B};$$

This equation shows that  $\alpha$  in equation (11) equals  $-\kappa$ ; however, this fact and equation (11) itself is no longer of any interest, since this equation is subsumed in the last equation. Equations (7), (12), and (13) are called the *Frenet–Serret formulas*. To summarize these formulas, we have

(14) 
$$\begin{aligned} \frac{d\mathbf{T}}{ds} &= \kappa \mathbf{N}, \\ \frac{d\mathbf{N}}{ds} &= -\kappa \mathbf{T} + \tau \mathbf{B}, \\ \frac{d\mathbf{B}}{ds} &= -\tau \mathbf{N}. \end{aligned}$$

#### The first three derivatives of r 3

As we mentioned above, we will indicate derivation with respect to t by prime. According to equations (5) and (3), we have

(15) 
$$\mathbf{r}' = |\mathbf{r}'|\mathbf{T} = s'\mathbf{T}$$

 $<sup>^{2.1}</sup>$ Every vector can be expressed as a linear combination of the basic unit vectors **T**, **N**, **B**; as  $d\mathbf{N}/ds$  is perpendicular to N, the coefficient of N in this linear combination is 0. <sup>2.2</sup>The member between the third and fourth equations

We can do further differentiations with respect to t by using equations (14), (4), and (3). We have

(16) 
$$\mathbf{r}'' = s''\mathbf{T} + s'\mathbf{T}' = s''\mathbf{T} + (s')^2 \frac{d\mathbf{T}}{ds} = s''\mathbf{T} + (s')^2\kappa\mathbf{N}.$$

Further, repeatedly using equations (15) and (14), we have

(17)  

$$\mathbf{r}^{\prime\prime\prime\prime} = s^{\prime\prime\prime\prime}\mathbf{T} + s^{\prime\prime}\mathbf{T}^{\prime} + \left(2s^{\prime}s^{\prime\prime}\kappa + (s^{\prime})^{2}\kappa^{\prime}\right)\mathbf{N} + (s^{\prime})^{2}\kappa\mathbf{N}^{\prime}$$

$$= s^{\prime\prime\prime\prime}\mathbf{T} + s^{\prime\prime}s^{\prime}\frac{d\mathbf{T}}{ds} + \left(2s^{\prime}s^{\prime\prime}\kappa + (s^{\prime})^{2}\kappa^{\prime}\right)\mathbf{N} + (s^{\prime})^{3}\kappa\frac{d\mathbf{N}}{ds}$$

$$= s^{\prime\prime\prime\prime}\mathbf{T} + s^{\prime\prime}s^{\prime}\kappa\mathbf{N} + \left(2s^{\prime}s^{\prime\prime}\kappa + (s^{\prime})^{2}\kappa^{\prime}\right)\mathbf{N} + (s^{\prime})^{3}\kappa(-\kappa\mathbf{T} + \tau\mathbf{B})$$

$$= \left(s^{\prime\prime\prime\prime} - (s^{\prime})^{3}\kappa\right)\mathbf{T} + \left(3s^{\prime\prime}s^{\prime}\kappa + (s^{\prime})^{2}\kappa^{\prime}\right)\mathbf{N} + (s^{\prime})^{3}\kappa\tau\mathbf{B}.$$

It is now easy to express  $\kappa$  and  $\tau$  in terms of derivatives with respect to t. Equations (15), (16), and (10) give

(18) 
$$\mathbf{r}' \times \mathbf{r}'' = (s')^3 \kappa \mathbf{B},$$

so using equation (3), we obtain that

(19) 
$$\kappa = \frac{|\mathbf{r}' \times \mathbf{r}''|}{|\mathbf{r}'|^3}$$

by noting that  $|\mathbf{B}| = 1$ . By equations (18) and (17) we have

$$(\mathbf{r}' \times \mathbf{r}'') \cdot \mathbf{r}''' = (s')^6 \kappa^2 \tau.$$

Hence, using equation (18) and noting that  $|\mathbf{B}| = 1$ , we obtain that

(20) 
$$\tau = \frac{(\mathbf{r}' \times \mathbf{r}'') \cdot \mathbf{r}'''}{|\mathbf{r}' \times \mathbf{r}''|^2}.$$

### 4 Examples and discussion

Since the curvature  $\kappa$  and the torsion  $\tau$  are defined in terms of the local coordinate frame **T**, **N**, **B** in arc-length parametrization, they only depend on the shape of the curve and not on the choice of the coordinate system x, y, z and the choice of the parameter t. Hence, for a curve that we want to calculate the curvature or the torsion, we may set up the coordinate system x, y, z and choose a parametrization that make these calculations especially simple.

### 4.1 The curvature of a circle

We consider the circle of radius R > 0 lying in the x, y plane, and centered at the origin. This circle can be parametrized by the equation

$$\mathbf{r} = R(\mathbf{i}\cos t + \mathbf{j}\sin t),$$

where  $\mathbf{i}$ ,  $\mathbf{j}$ , and  $\mathbf{k}$  are the unit coordinate vectors in the directions of the positive x, y, and z axes, respectively. We have

$$\mathbf{r}' = R(-\mathbf{i}\sin t + \mathbf{j}\cos t)$$

 $\mathbf{r}'' = -R(\mathbf{i}\cos t + \mathbf{j}\sin t).$ 

Hence

and

$$\mathbf{r}' \times \mathbf{r}'' = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ -R\sin t & R\cos t & 0 \\ -R\cos t & -R\sin t & 0 \end{vmatrix} = R^2(\sin^2 t + \cos^2 t)\,\mathbf{k} = R^2\,\mathbf{k}.$$

We also have

$$|\mathbf{r}'| = R\sqrt{\cos^2 t + \sin^2 t} = R.$$

Hence equation (19) gives that

$$\kappa = \frac{R^2}{R^3} = \frac{1}{R}.$$

Thus, the curvature of a circle is the reciprocal of the radius. For this reason, given any curve,  $1/\kappa$  is called the radius of curvature; it is the radius of the *osculating circle*: given an curve by the equation  $\mathbf{r} = \mathbf{F}(t)$ , the osculating circle at a point corresponding to the parameter value  $t = t_0$  (i.e., at the point with position vector  $\mathbf{r}_0 = \mathbf{F}(t_0)$ ) is a circle with equation  $\mathbf{r} = \mathbf{G}(t)$  at the for which

(21) 
$$\mathbf{G}(t_0) = \mathbf{F}(t_0), \quad \mathbf{G}'(t_0) = \mathbf{F}'(t_0), \text{ and } \mathbf{G}''(t_0) = \mathbf{F}''(t_0).$$

For the existence of such a circle, one needs to assume that  $\mathbf{F}'(t_0) \neq 0$  and  $\mathbf{F}''(t_0) \neq 0$ . The case that  $\mathbf{F}'(t_0) = 0$  is a case of bad parametrization, when the curve may or may not have a tangent line and a curvature, but the equation is not suitable for determining the tangent line or the curvature. In this case, one needs to re-parametrize the curve in such a way that the derivative at the point with position vector  $\mathbf{F}(t_0)$  is not zero.<sup>4.1</sup> If  $\mathbf{F}'(t_0) \neq 0$  but  $\mathbf{F}''(t_0) = 0$ , the curvature is 0, and the osculating circle degenerates into a straight line; in fact, the tangent line can be considered the osculating "circle" in this case, and one may say that the corresponding radius of curvature is infinite.

### 4.2 The curvature and the torsion of a helix

A helix in the standard position can be described by the equation

$$\mathbf{r} = \mathbf{i} R \cos t + \mathbf{j} R \sin t + ct \, \mathbf{k} \qquad (R > 0).$$

We have

$$\mathbf{r}' = -\mathbf{i} R \sin t + \mathbf{j} R \cos t + c \mathbf{k},$$
  

$$\mathbf{r}'' = -\mathbf{i} R \cos t - \mathbf{j} R \sin t,$$
  

$$\mathbf{r}''' = \mathbf{i} R \sin t - \mathbf{j} R \cos t.$$

Therefore

$$|\mathbf{r}'| = \sqrt{R^2(\sin^2 t + \cos^2 t) + c^2} = \sqrt{R^2 + c^2}$$

Furthermore,

$$\mathbf{r}' \times \mathbf{r}'' = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ -R\sin t & R\cos t & c \\ -R\cos t & -R\sin t & 0 \end{vmatrix} = \mathbf{i} cR\sin t - \mathbf{j} cR\cos t + R^2(\sin^2 t + \cos^2 t) \mathbf{k}$$
$$= \mathbf{i} cR\sin t - \mathbf{j} cR\cos t + R^2 \mathbf{k}.$$

 $^{4.1}$ Such a parametrization may not exist. If there is a suitable re-parametrization, the re-parametrization with respect to arc length will work. It is, however, possible, that the derivative of the arc-length parametrization at the given point does not exist – in which case there is no smooth re-parametrization at the point.

Thus

$$|\mathbf{r}' \times \mathbf{r}''| = \sqrt{c^2 R^2 (\cos^2 t + \sin^2 t) + R^4} = R\sqrt{c^2 + R^2}$$

and

$$(\mathbf{r}' \times \mathbf{r}'') \cdot \mathbf{r}''' = R\sqrt{c^2 + R^2} = cR^2 \sin^2 t + cR^2 \cos^2 t = cR^2.$$

Hence, using formula (19) we obtain

$$\kappa = \frac{R\sqrt{c^2 + R^2}}{(R^2 + c^2)^{3/2}} = \frac{R}{R^2 + c^2}.$$

Similarly, using formula (20)

$$\tau = \frac{cR^2}{R^2(c^2 + R^2)} = \frac{c}{R^2 + c^2}.$$

An osculating curve to a given curve  $\mathbf{r} = \mathbf{F}(t)$  is a curve  $\mathbf{r} = \mathbf{G}(t)$  satisfying equations (21); these equations can also be described by saying that the curves  $\mathbf{r} = \mathbf{F}(t)$  and  $\mathbf{r} = \mathbf{G}(t)$  have a second order contact at the given point. One can generalize this to an arbitrary integer n by saying that the curve  $\mathbf{r} = \mathbf{F}(t)$  and  $\mathbf{r} = \mathbf{F}(t)$  have an order n contact for a given parameter value  $t = t_0$  if  $\mathbf{F}'(t_0) \neq 0$ and<sup>4.2</sup>

(22) 
$$\mathbf{G}^{(k)}(t_0) = \mathbf{F}^{(k)}(t_0) \quad \text{for all } k \text{ with } 0 \le k \le n.$$

The osculating plane is the plane spanned by the vectors  $\mathbf{T}$  and  $\mathbf{N}$ . The osculating circle lies in this place. The osculating plane has a second order contact with the curve at the point given by a parameter value  $t = t_0$ . More generally, if  $\mathbf{F}'(t_0) \neq 0$  and  $\mathbf{F}''(t_0) \neq 0$ , then any plane curve that has a second order contact with the curve  $\mathbf{r} = \mathbf{F}(t)$  at the parameter value  $t = t_0$  lies entirely in the osculating plane. If  $\mathbf{F}''(t_0) = 0$  then the osculating plane is not determined since  $\kappa = 0$  in this case so the vector  $\mathbf{N}$  is not determined (cf. equations (19) and (7) to see this). The torsion expresses the speed with which the osculating place turns as the arc-length parameter changes (indeed, this follows from the third equation in (14), since  $\mathbf{B}$  is normal to the osculating plane).

The derivation of the Frenet–Serret formulas (14) shows the theoretical usefulness of arc-length parametrization. Re-parametrizing a curve with respect to arc-length is rarely done in practice, since the integrals involved cannot usually be evaluated, and a more useful procedure is to rewrite the formulas derived with arc-length parametrization in terms of the original parameter, as was done in formulas (19) and (20).

<sup>&</sup>lt;sup>4.2</sup>This condition just mentioned may be dropped if one is only interested in the curve as a moving points. If  $F'(t_0) = 0$  then this condition expresses only that the points near the time  $t = t_0$  have a "higher order closeness," but since both points stop moving at this time, this has no implication for the geometry of the two curves.